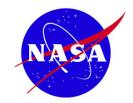
Novel uses of DNS with turbulent separation for RANS models

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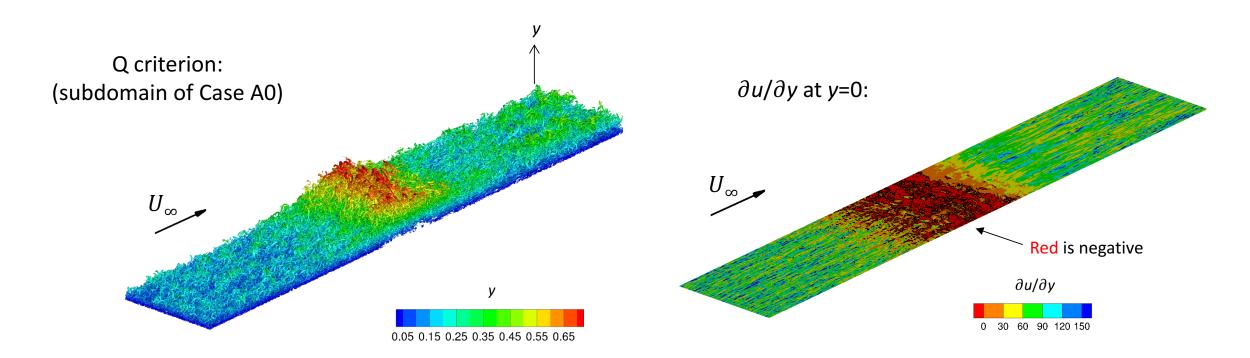
Outline

□ Flow: *spatial separation bubbles*

- Extending Spalart & Coleman 97 (Eur J. Mech. B/Fluids 16(2):169-189)
- Five cases: with/without sweep, sudden/gradual pressure gradient (PG), 2X Reynolds number; larger domain
- □ Strategy use DNS data for...
 - "Conventional" uses Test turbulence theory and RANS modeling...
 - \circ <u>Concepts</u> (Stratford scaling at $C_f = 0$ stations)
 - <u>Predictions</u> (SA, SST, RSM, ...) of separation/reattachment locations
 - "Novel" uses Diagnose <u>Effective eddy viscosity</u> for...
 - \circ Full Reynolds-stress tensor
 - RANS model counterparts (check correlation to separation predictions)
 - Frozen-field solutions (check constitutive relationships)
 - Only wall-parallel components, for cases with sweep
 - Explore idea of a different eddy viscosity in the *x*-*z* plane than in the *y* direction

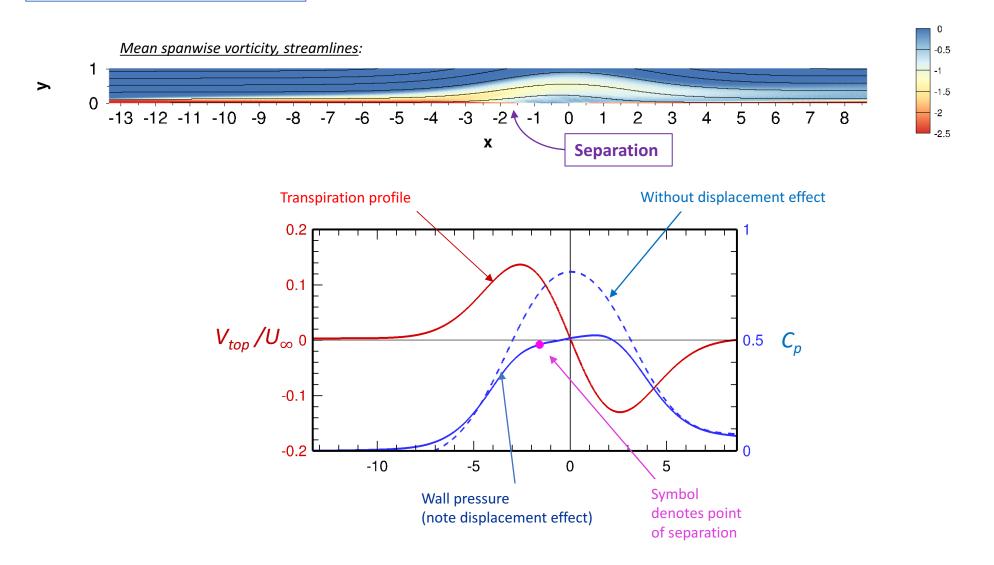
Summary/Open questions

Flow – <u>Visualization</u>: DNS of PG-induced flat-plate separation bubbles

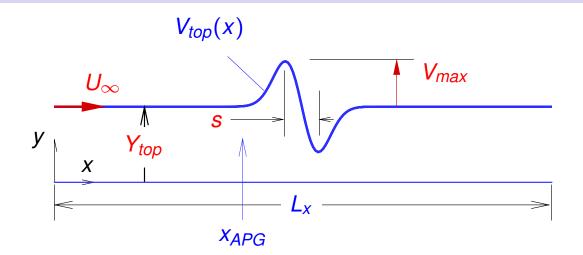


Flow – <u>Mean</u>: DNS of PG-induced flat-plate separation bubbles...

Case CO (gradual APG, Re=80000):

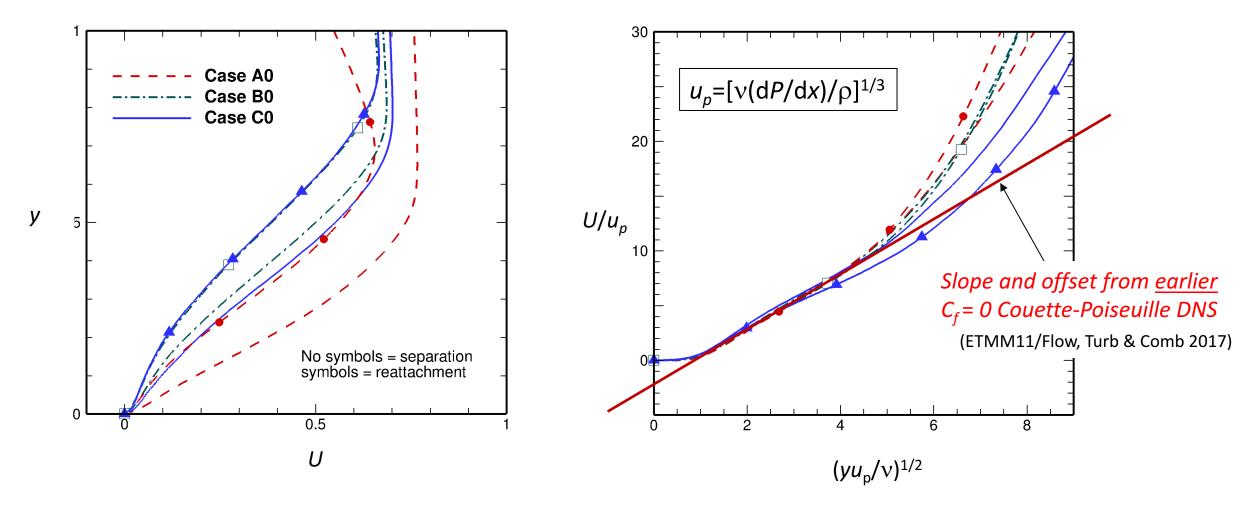


Cases



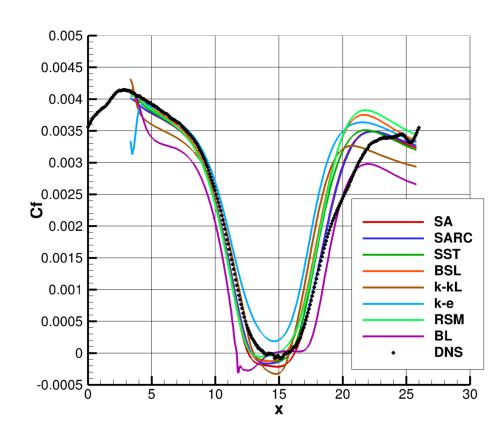
Case	arctan $\left(\frac{W_{\infty}}{U_{\infty}}\right)$	s/Y _{top}	V_{max}/U_{∞}	$R_{ heta} _{x_{APG}}$	$N_x \cdot N_y \cdot N_z$
SC97	0°	1.7	0.435	550	$0.03 imes 10^{9}$
A0	0 °	1.7	0.40	1400	$0.98 imes10^9$
B0	0 °	5.2	0.13	980	$0.98 imes10^9$
C0	0 °	5.2	0.13	2200	$4.72 imes10^9$
A35	35°	1.7	0.40	1350	$1.97 imes10^9$
B35	35 °	5.2	0.13	835	$1.97 imes10^9$

SC97: $L_x/Y_{top} = 10$, $L_z/Y_{top} = 1.4$ New cases: $L_x/Y_{top} = 26$, $L_z/Y_{top} = 4.0$ "Conventional" strategy – Part 1 of 2: Test <u>theoretical concepts</u>: Stratford zero-stress velocity scaling $(U \sim \sqrt{y})$ Profiles at separation and reattachment (all three unswept cases)

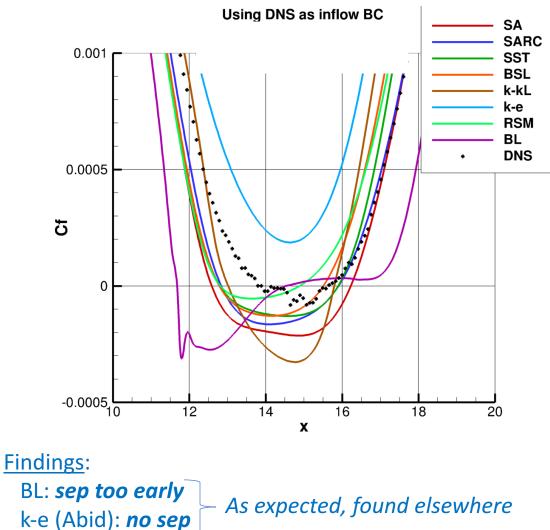


<u>Implication</u>: Prolonged $C_f = 0$ region **NOT** required! 6

"Conventional" strategy – Part 2 of 2: Test <u>CFD RANS predictions</u>: Skin friction profiles/separation & reattachment locations



Solutions via CFL3D, using DNS as inflow BC

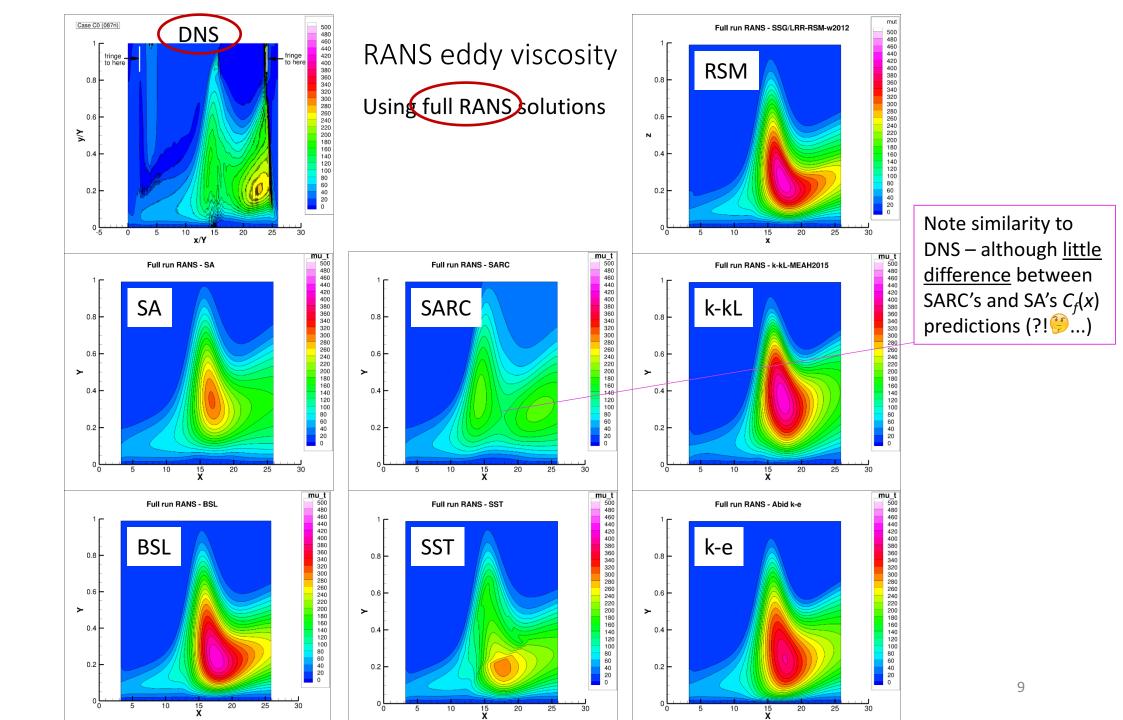


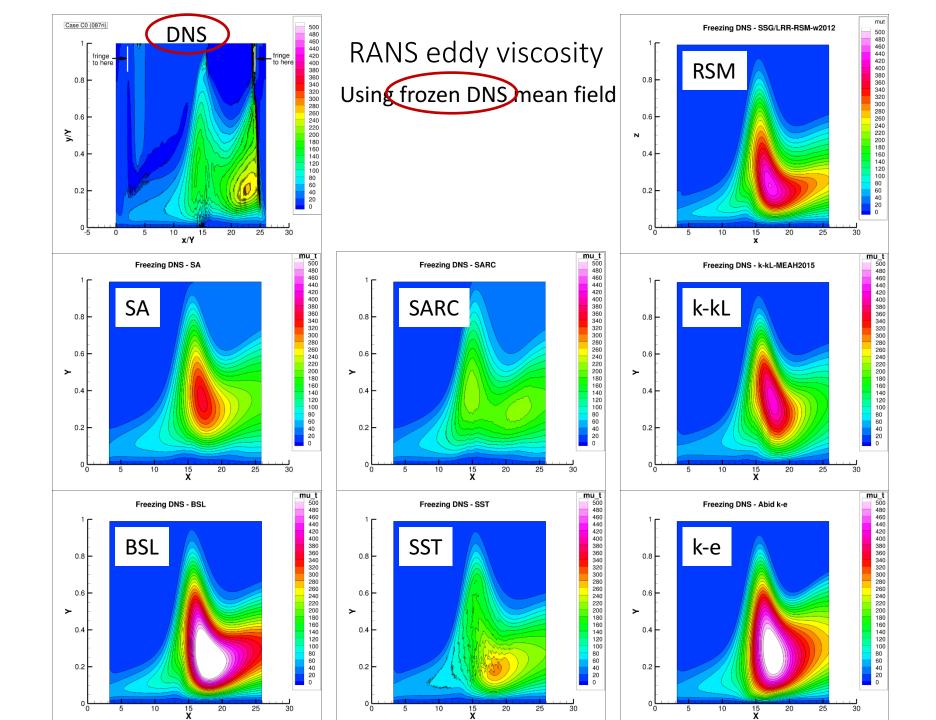
SA/SST/RSM/etc: *somewhat too early and too deep*, and *together* (why?)...⁷ (Recovery difficult in its own right)

"Novel" strategy - Effective eddy viscosity

$$\nu_{t,eff} \equiv \frac{\mathcal{P}_{TKE}}{2\mathcal{S}^2} = \frac{-u_i' u_j' S_{ij}}{2S_{k\ell} S_{k\ell}}, \text{ where } S_{ij} = \frac{1}{2} \left(\frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right).$$

- Follows from Boussinesq approximation and assumed dependence of eddy viscosity on TKE production (to give correct mean-to-turbulence energy transfer)
- Corresponds to least-squares fit of Reynolds stress tensor by scalar eddy viscosity
- Available from DNS, convenient RANS-model diagnostic tool for Machine Learning?
 Full RANS-model solutions (highlight critical regions)
 - Models solved in "frozen" DNS fields (check constitutive relationship)





Effective eddy viscosity (cont'd)...

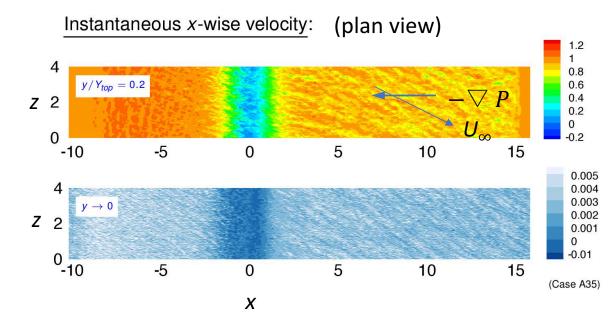
<u>Comment</u>: Effective eddy viscosity tends to be <u>higher</u> for frozenfield solutions than for normal/coupled RANS solutions. *Why?...*

<u>Question</u>: Why did such large differences in eddy viscosity in models produce relatively little difference in $C_f(x)$ predictions? *Near-inviscid behavior in APG region? Common model structure? TBD...*

Effective Eddy Viscosity in Different Directions

- ▶ In the effective eddy viscosity shown earlier, the wall-normal terms dominate: $-\overline{u'v'}$ and S_{12}
 - The RANS models are made to favor the wall-normal diffusion
- ► We can define a "lateral" eddy viscosity, possibly quite different from the wall-normal eddy viscosity...
 - o ...And probably larger! Evidence from wall jets, and turbulent wedges in a laminar BL
- ► The first idea is to apply the formula, but only to the strain and stresses in the x-z plane
 - \circ Recall that in the past, eddy viscosity in a single direction has been defined, e.g., $-\overline{u'v'}$ / (dU/dy)
- ▶ 2D flows don't have an "interesting" strain S_{11} in the x direction...
- But the swept APG flow has a meaningful strain field in the x-z plane, allowing a non-trivial " $v_{t,xz}$ " to be defined

Consider APG-induced separation with sweep...

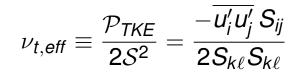


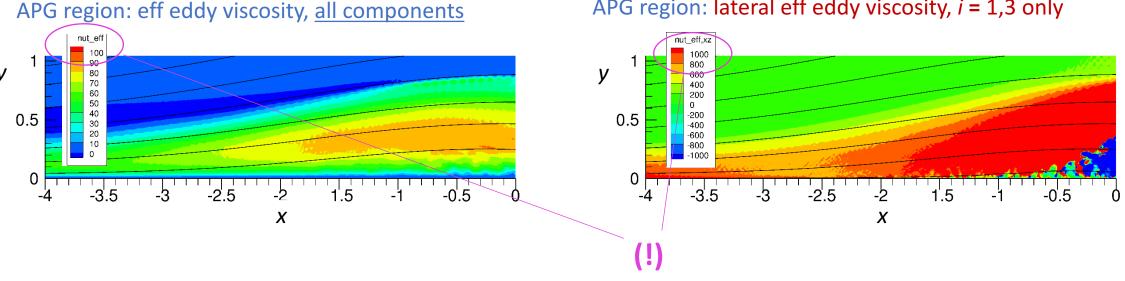
...and examine

$$u_{t,\text{eff}} \equiv rac{\mathcal{P}_{TKE}}{2\mathcal{S}^2} = rac{-\overline{u'_i u'_j} \, \mathcal{S}_{ij}}{2\mathcal{S}_{k\ell} \mathcal{S}_{k\ell}}.$$

for *i* = 1,3 **only**...

Effective eddy viscosity in wall-parallel plane: *i* = 1,3 only...





APG region: lateral eff eddy viscosity, *i* = 1,3 only

- Very different behavior of effective wall-parallel eddy viscosity may lead to new modeling ideas
 - This eddy viscosity is indeed much larger
 - And has strong negative excursion at separation
- We would have a constitutive relation that incorporates the wall-normal vector
- Role for/input to Machine Learning?

Summary/Open questions

- DNS of spatial separation used to address modeling issues, in conventional and new ways
 - New family of cases, with much "bigger data" than in 1997
- Effective-eddy-viscosity "target" from DNS highlights:
 - model limitations
 - wide variations in eddy viscosity between models (only around separation)
- Correlation between model's separation prediction and eddy-viscosity fields not strong is it a feature of flow or model?
- Proposed "wall-parallel eddy viscosity" exhibits unexpected behavior
 - Very preliminary concept
- Paper(s) in preparation, data to be made available soon