Challenges for RANS Models in Turbomachinery Flows

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Turbulence Modeling Symposium University of Michigan, July 11-13, 2017



Outline

- Motivation
 - Role of CFD in jet engine turbomachinery
- Some areas of particular interest for RANS model improvement
 - Flow separation
 - Endwall features corner separation & clearance flows
 - Shock-boundary layer interaction
 - Thermal mixing
- Potential avenues for future advances



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Motivation

• Role of CFD in jet engine turbomachinery?



Becoming part of design-cycle; Prediction, not post-diction

- Careful multi-row U-RANS represents state-of-the-art
- Well-recognized limitations when it comes to transition, roughness, mixing, shock/BL, stress-anisotropy ...

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Motivation





Motivation

Reynolds numbers lower than for external aero



Allows brute-force wall-resolved LES of airfoils (<100K CPUhours)</p>

With endwalls, even for a single-row blade/vane, computational cost grows to millions of CPUhours

Use high-fidelity CFD to advance hybrid methods & RANS models?



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Flow separation

Separation onset – Buice diffuser

- In turbomachinery applications, designers avoid airfoil and endwall separation, however, at off design conditions, small pockets of separation start appearing
- Separation onset particularly hard to predict strongly influenced by the state of the approaching boundary layer (transition, impact of pressure gradient)
- > RANS models typically predict onset too early, even in well controlled conditions:





Flow separation

Separation onset – Buice diffuser

Interesting new results that improve both separation onset and reattachment using elliptic blending lag model (k-ε-φ model) from UK; similar improvement for periodic hill and 2D-curved backward facing step – does this translate to airfoils/endwalls?



Sylvain Lardeau and Flavien Billard, Development of an elliptic-blending lag model for industrial applications, AIAA Paper AIAA-2016-1600.

Recent study on LES and RANS for bumps of varying height by Prof. Durbin's team at Iowa State University:







Flow separation

Reattachment – NASA hump

- With RANS, reattachment also usually delayed, and separation length over predicted by 20-30%
- Reports in literature on improved prediction of separation shear layer using hybrid RANS/LES (Shur, Spalart, Strelets & Travin, FTC, 2014)
 - Need to resolve/synthesize turbulent eddies in the oncoming boundary layer









KW88S

Ecole Centrale de Lyon compressor cascade

- RANS models tend to over-predict hub-corner stall events in axial compressors
- ECL team performed wall-resolved LES which matched the experimental data very well – is it really necessary to resolve all the boundary layers on endwall & airfoils?



No technical data subject to the EAR or the ITAR.

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Ecole Centrale de Lyon compressor cascade

- Maybe resolving eddies in the corner separation region would help try to apply hybrid RANS/LES!
- Results improved over RANS further downstream of TE, but not for section1



Total pressure loss coefficient downstream of TE

(b) LES outlet section 1

(e) LES outlet section 2

(h) LES outlet section 3

LES

DDES

Corner



SST

Ecole Centrale de Lyon compressor cascade

- Bi-modal nature of separation observed in experiments
- Horse-shoe vortex at LE also exhibits bi-modal behavior how about resolving the horse-shoe vortex region in addition to the corner separation region?





Ecole Centrale de Lyon compressor cascade

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14

Endwall features – clearance vortex

Virginia Tech experiments (Devenport et al.)

- Compressor cascade with endgap; data for stationary and moving endwall
- Detailed velocity and turbulence measurements in the wake and clearance vortex

 at multiple stations downstream of trailing edge





Endwall features – clearance vortex

Virginia Tech experiments (Devenport et al.)

Results indicate that RANS models are predicting trajectory of the vortex incorrectly, in particular for stationary endwall



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Endwall features – clearance vortex

Johns Hopkins University experiments (Katz et al.)

- One-and-a-half stage axial compressor, based on NASA LSAC; includes a configuration with casing treatment (axial, semi-circular, skewed grooves at LE)
- JHU refractive index-matching liquid facility allows for detailed measurement of flow in tip region where clearance vortex originates



Yuanchao Li, Huang Chen, and Joseph Katz, Measurement and Characterization of Turbulence in the Tip Region of an Axial Compressor Rotor, ASME Paper GT2017-64114. Huang Chen, Yuanchao Li, Subhra Koley, Nick Doeller, and Joseph Katz, An Experimental Study of Stall Suppression and Associated Changes to the Flow Structures in the Tip Region of an Axial Low-Speed Rotor by Axial Casing Grooves, ASME Paper GT2017-65099.

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Shock-boundary layer interaction

Bachalo-Johnson bump

- Shock-induced boundary layer separation represents another challenge for RANS models, even for hybrid RANS/LES (Spalart et al, ETMM-11, 2016)
 - Use DNS from ETMM-11 to inform RANS modeling, via Machine Learning?
- SST limiter calibrated to capture the separation for Bachalo-Johnson bump:



> However, in other cases SST too aggressive (e.g. 24° compression corner)



Shock-boundary layer interaction

NASA Stage 35-37

> At off-design conditions, SST limiter designed to capture shock-induced boundary layer separation starts causing flow to separate elsewhere leading to an early rollover of the stage characteristic





Suction side loading / nominal condition

Thermal mixing

Co-annular duct experiment (NASA, 2012)



- Testing conducted at the NASA AAPL Hot Flow Jet Exhaust Rig
- Data taken for 26 conditions over a large range of shear layer conditions
 - Temperature ratios (LTR) of 0.31 to 0.7
 - Total pressure ratios (LPR) of 0.92 to 1.05
 - Velocity difference (dU/U) of 0.0 to 1.0

Robert H. Bush, Harry C. M. Culver, Dave Weissbein and Nicholas J. Georgiadis, Low Velocity Difference Thermal Shear Layer Mixing Rate Measurements, AIAA Paper AIAA-2013-1074.





Thermal mixing

Co-annular duct experiment (NASA, 2012)

> RANS models tend to under predict the mixing and outer wall temperatures (η_{mix}):



PK3 model – a density-gradient based term is added to production term P_k in the k-epsilon region of SST model:

$$P_{k} = 2 \mu_{t} S_{ij} S_{ij} + \left| \mu_{t} \left| \frac{\nabla \rho}{\rho} \times u \right|^{2} \right|$$

Robert H. Bush, Turbulence Model Extension for Low Speed Thermal Shear Layers, AIAA Paper AIAA 2014-2086.

> NVT model: PK3 model + reduction in Pr_T to 0.5 in k-epsilon region of SST model



Thermal mixing

Co-annular duct experiment (UTRC, 2017)

- > New experiments and high-fidelity LES computations at UTRC in 2016/2017
 - Temperature (and turbulence?) profiles at multiple axial stations
 - Aiming to separate the contribution from changes to turbulent kinetic energy and turbulent heat flux
- Use LES to guide RANS model corrections:
 - LES predicts much more rapid mixing just downstream of splitter trailing edge via 3D vortical structures
 - Reminiscent of pressure side trailing edge slot cooling







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- Machine learning for RANS model improvement
 - Data extraction combined with phenomenological modeling (Prof. Durbin's group)
 - If capturing unsteadiness / large (3D) turbulent structures matters, can RANS overcome that?
- Hybrid RANS/LES modeling
 - Where does it offer an advantage in turbomachinery flows?
- LES with wall-models to reduce cost
 - Challenge: boundary layer development a critical feature in turbomachinery!



- RANS model improvement focus:
 - Transition modeling and suppression of turbulence (relaminarization) in accelerating boundary layers
 - Roughness induced boundary layer thickening and separation
 - Systematic prediction of impact of shock-boundary layer interactions on the state of boundary layer
 - Additional terms in the k equation for compressible flows with large variations in density
 - Turbulent heat flux model beyond GGDH with eddyviscosity models?

